

COL865: Special Topics in Computer Applications

Physics-Based Animation

14 – Fluid simulation on grids II

Review

Navier-Stokes equations for fluid velocity $\mathbf{u}(\mathbf{x}, t)$:

$$\frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla) \mathbf{u} = \rho^{-1} (-\nabla p + \mu \nabla^2 \mathbf{u} + \mathbf{f}_{\text{ext}})$$

$$\nabla \cdot \mathbf{u} = 0$$

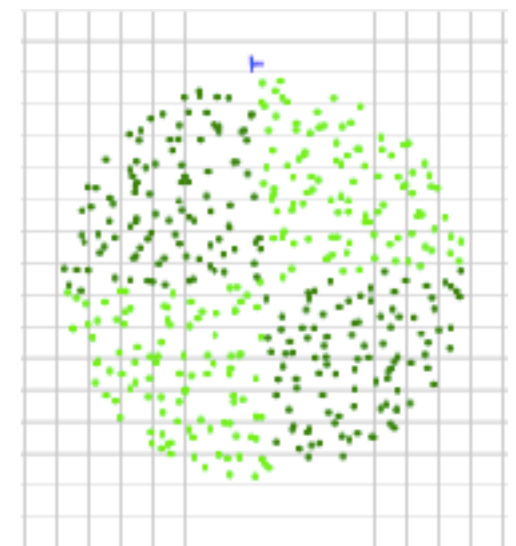
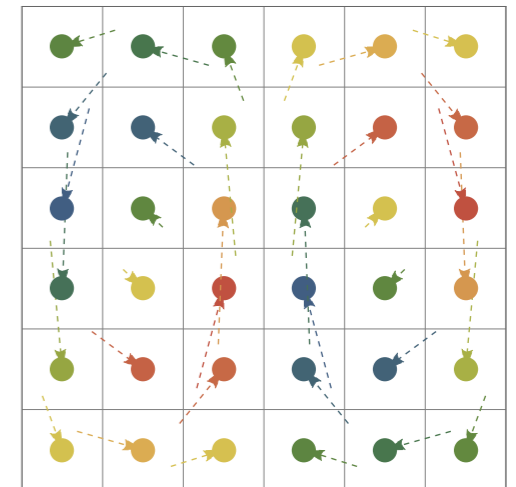
Solve on grid via *splitting*:

- **Advection**: $\mathbf{u}^{(1)} = \text{advect}(\mathbf{u}^n, \mathbf{u}^n, \Delta t)$
- **Body forces**: $\mathbf{u}^{(3)} = \mathbf{u}^{(2)} + \mathbf{f}_{\text{ext}} \Delta t$
- **Viscosity**: $\mathbf{u}^{(2)} = \mathbf{u}^{(1)} + \nu \nabla^2 \mathbf{u} \Delta t$
- **Pressure**: $\mathbf{u}^{n+1} = \mathbf{u}^{(3)} - \nabla p \Delta t$ so that $\nabla \cdot \mathbf{u}^{n+1} = 0$

Advection

$$D\mathbf{u}/Dt = \partial\mathbf{u}/\partial t + (\mathbf{u} \cdot \nabla) \mathbf{u} = 0$$

- ***Finite differences***
(time step limited by CFL condition)
- ***Semi-Lagrangian***
- ***Particle-based***: PIC, FLIP, APIC



Pressure

$$\mathbf{u}^{n+1} = \tilde{\mathbf{u}} - \nabla p \Delta t,$$

$$\nabla \cdot \mathbf{u}^{n+1} = 0$$

$$\Rightarrow \nabla \cdot \tilde{\mathbf{u}} - \nabla^2 p \Delta t = 0$$

$\tilde{\mathbf{u}}$

=

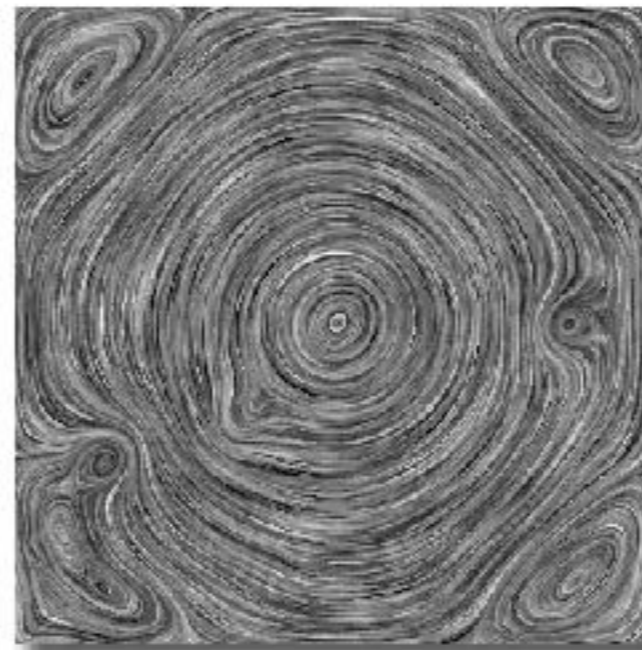
\mathbf{u}^{n+1}

+

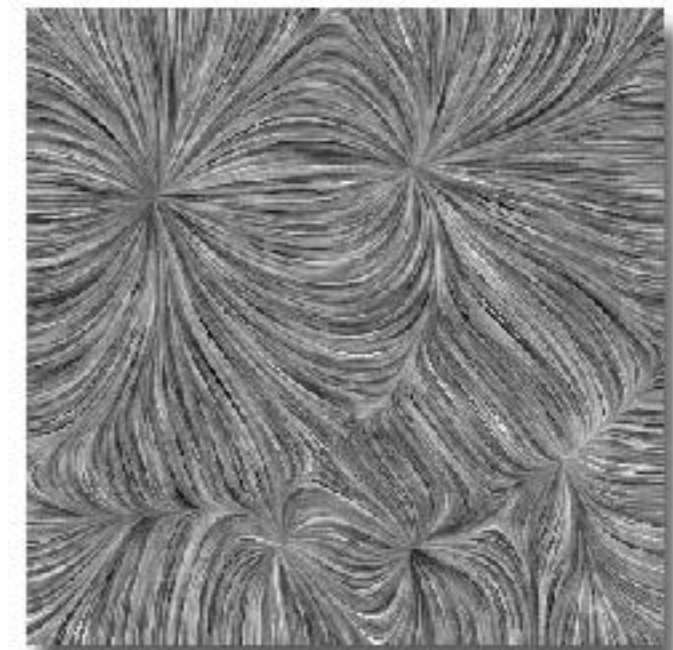
∇p



=



+

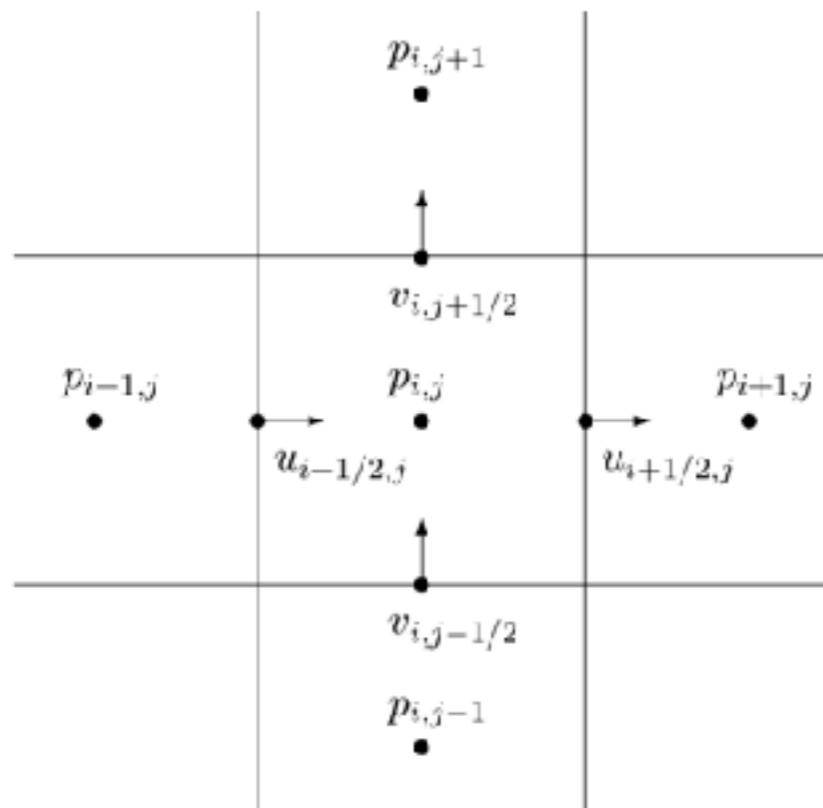


[Tong et al. 2003]

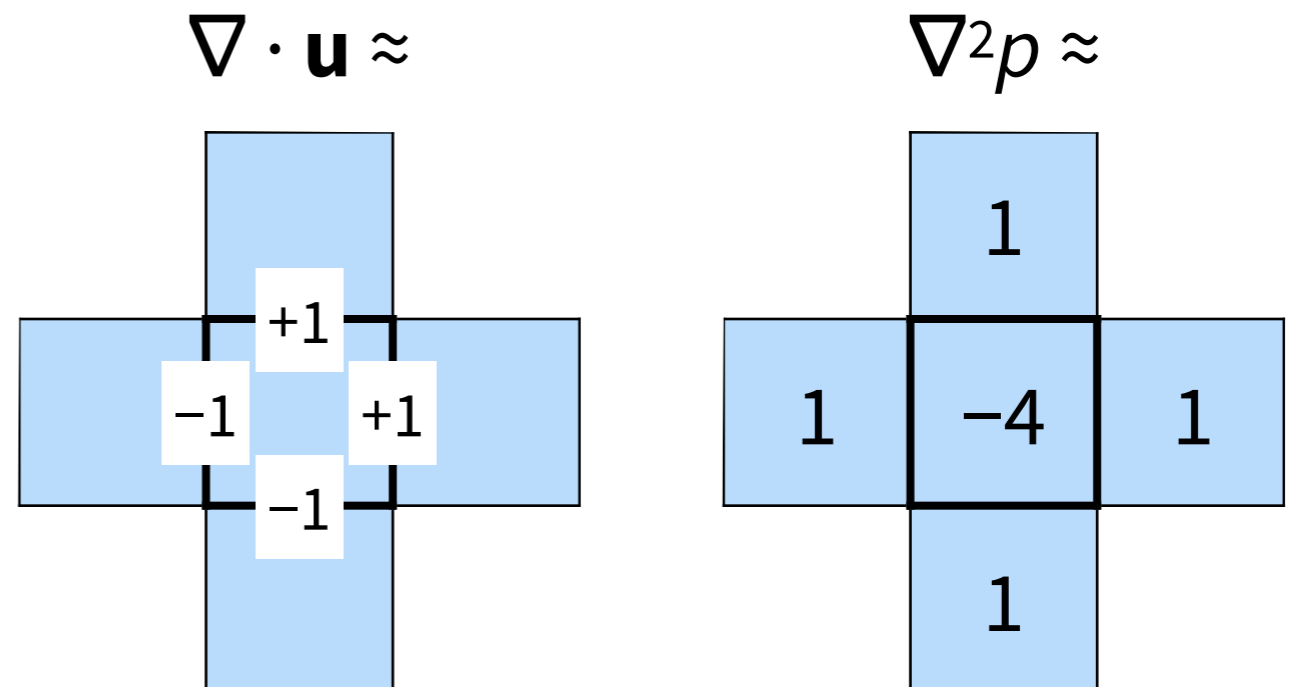
Pressure on staggered grids

$$(\nabla \cdot \mathbf{u})_{i,j} \approx (u_{i+1/2,j} - u_{i-1/2,j})/\Delta x + (v_{i,j+1/2} - v_{i,j-1/2})/\Delta x$$

$$(\nabla^2 p)_{i,j} \approx (p_{i-1,j} + p_{i+1,j} + p_{i,j-1} + p_{i,j+1} - 4p_{i,j})/\Delta x^2$$



[Bridson & Müller-Fischer]



The pressure system

$$\nabla^2 p \Delta t = \nabla \cdot \tilde{\mathbf{u}}$$

1. Compute $(\nabla \cdot \tilde{\mathbf{u}})_{i,j} = d_{i,j}$ on cell centers

2. Put pressure values in a vector \mathbf{p} :

$(\nabla^2 p \Delta t)_{i,j}$ becomes a linear operator $\mathbf{A} \mathbf{p}$

$$\begin{bmatrix} \ddots & & & & & & & & \\ & \ddots & & & & & & & \\ & & 1 & & & & & & \\ & & & 1 & & & & & \\ & & & & -4 & & & & \\ & & & & & 1 & & & \\ & & & & & & \ddots & & \\ & & & & & & & \ddots & \end{bmatrix} \begin{bmatrix} \vdots \\ p_{i-1,j} \\ \vdots \\ p_{i,j-1} \\ p_{i,j} \\ p_{i,j+1} \\ \vdots \\ p_{i+1,j} \\ \vdots \end{bmatrix} = \begin{bmatrix} \vdots \\ (\nabla \cdot \mathbf{u})_{i,j} \\ \vdots \end{bmatrix}$$

(taking $\Delta t = \Delta x = 1$)

3. Solve $\mathbf{A} \mathbf{p} = \mathbf{d}$ for \mathbf{p}

The pressure system

$$\nabla^2 p \Delta t = \nabla \cdot \tilde{\mathbf{u}}$$

1. Compute $(\nabla \cdot \tilde{\mathbf{u}})_{i,j} = d_{i,j}$ on cell centers
2. Put pressure values in a vector \mathbf{p} :
 $(\nabla^2 p \Delta t)_{i,j}$ becomes a linear operator $\mathbf{A} \mathbf{p}$

$$\begin{bmatrix}
 \ddots & & & & & & \\
 & \ddots & & & & & \\
 & & -1 & & & & \\
 & & & -1 & 4 & -1 & \\
 & & & & -1 & & \\
 & & & & & \ddots & \\
 & & & & & & \ddots
 \end{bmatrix}
 \begin{bmatrix}
 \vdots \\
 p_{i-1,j} \\
 \vdots \\
 p_{i,j-1} \\
 p_{i,j} \\
 p_{i,j+1} \\
 \vdots \\
 p_{i+1,j} \\
 \vdots
 \end{bmatrix}
 =
 \begin{bmatrix}
 \vdots \\
 -(\nabla \cdot \mathbf{u})_{i,j} \\
 \vdots
 \end{bmatrix}$$

Negate for positive definiteness

3. Solve $\mathbf{A} \mathbf{p} = \mathbf{d}$ for \mathbf{p}

Solving the pressure system

- Easy way: ***Gauss-Seidel iterations***

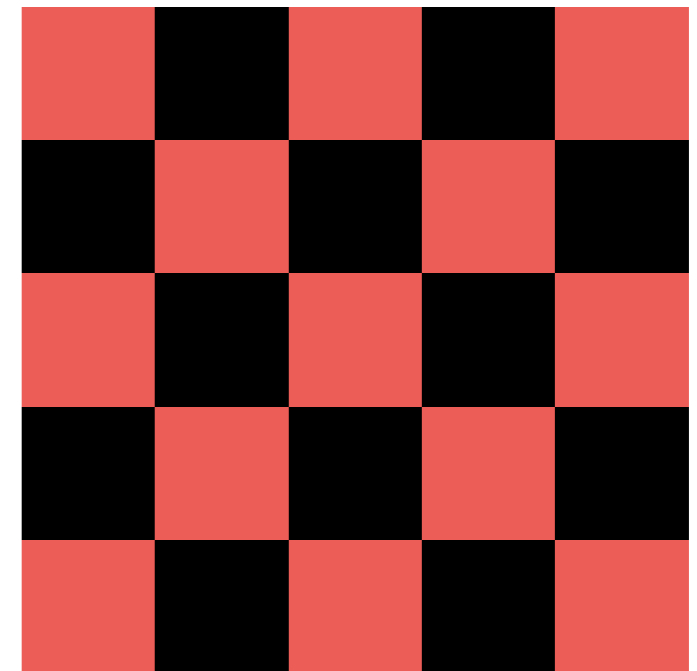
$$p_{i-1,j} + p_{i+1,j} + p_{i,j-1} + p_{i,j+1} - 4 p_{i,j} = (\nabla \cdot \tilde{\mathbf{u}})_{i,j}$$

$$\Rightarrow p_{i,j} = \frac{1}{4} (p_{i-1,j} + p_{i+1,j} + p_{i,j-1} + p_{i,j+1} + (\nabla \cdot \tilde{\mathbf{u}})_{i,j})$$

Parallelization via ***red-black ordering***

- Better way: ***Preconditioned conjugate gradient method***

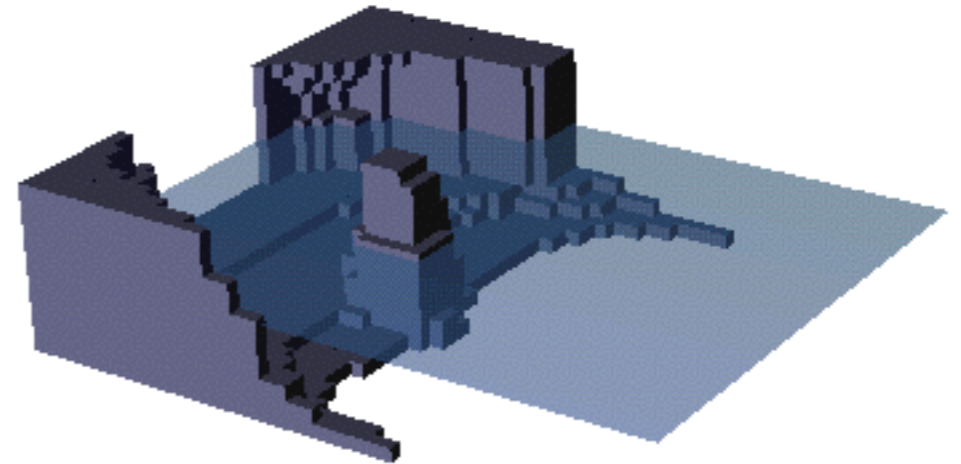
See Bridson & Müller-Fischer, Ch 4.3



Boundaries

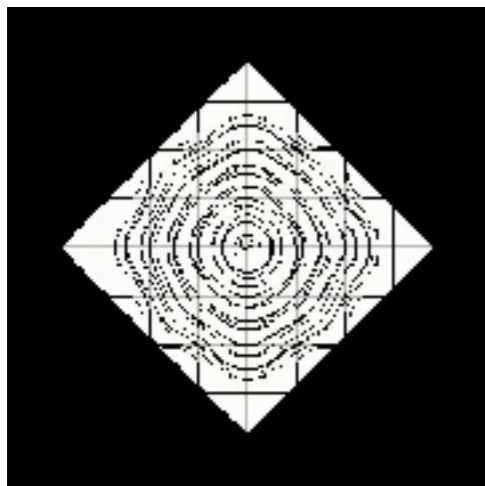
Static obstacles:

- Solid faces have $\mathbf{u} \cdot \mathbf{n} = 0$, do not contribute to $\nabla \cdot \mathbf{u}$
- Pressure shouldn't change $\mathbf{u} \cdot \mathbf{n}$, so $\nabla p \cdot \mathbf{n} = 0$



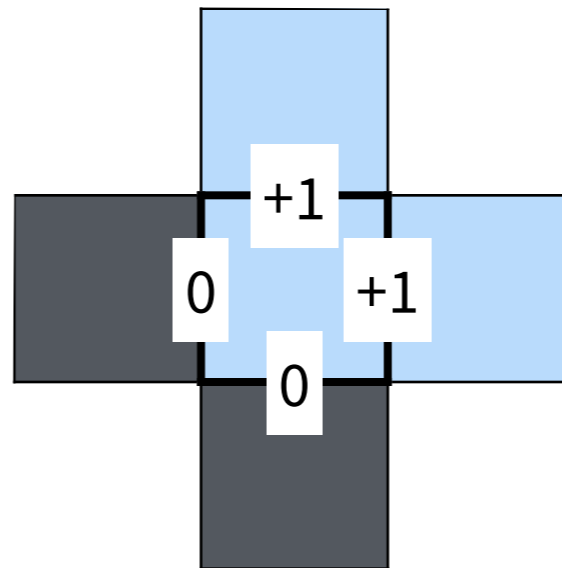
[Foster & Metaxas 1996]

Limitation: Sloped boundaries are jagged

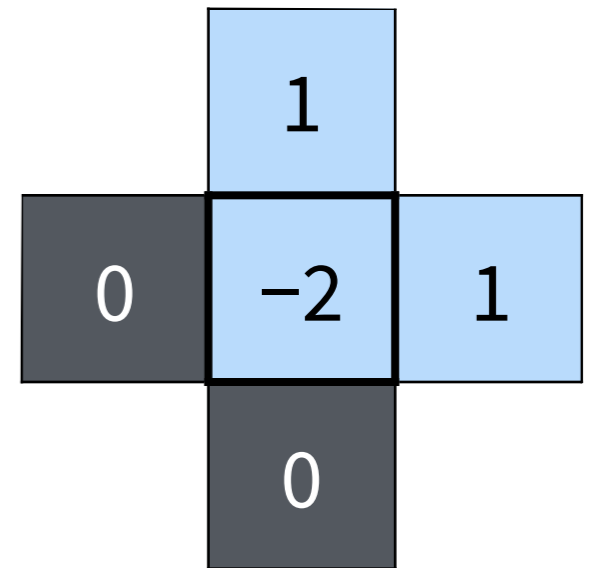


[Batty et al. 2007]

$$\nabla \cdot \mathbf{u} \approx$$



$$\nabla^2 p \approx$$



Putting it all together

A basic fluid simulator

Create staggered grid for domain, flag cells as solid/fluid

For each time step:

1. Compute $\tilde{\mathbf{u}} = \text{advect}(\mathbf{u}^n, \mathbf{u}^n, \Delta t)$
2. Add body forces: $\tilde{\mathbf{u}} += \rho^{-1} \mathbf{f}_{\text{ext}} \Delta t$
3. Do viscosity step if desired
4. Set $\mathbf{u}^{n+1} = \text{project}(\tilde{\mathbf{u}})$

Suppose $\mathbf{u}^0 = \mathbf{0}$, $\mathbf{f}_{\text{ext}} = \rho \mathbf{g} \dots$ What happens?

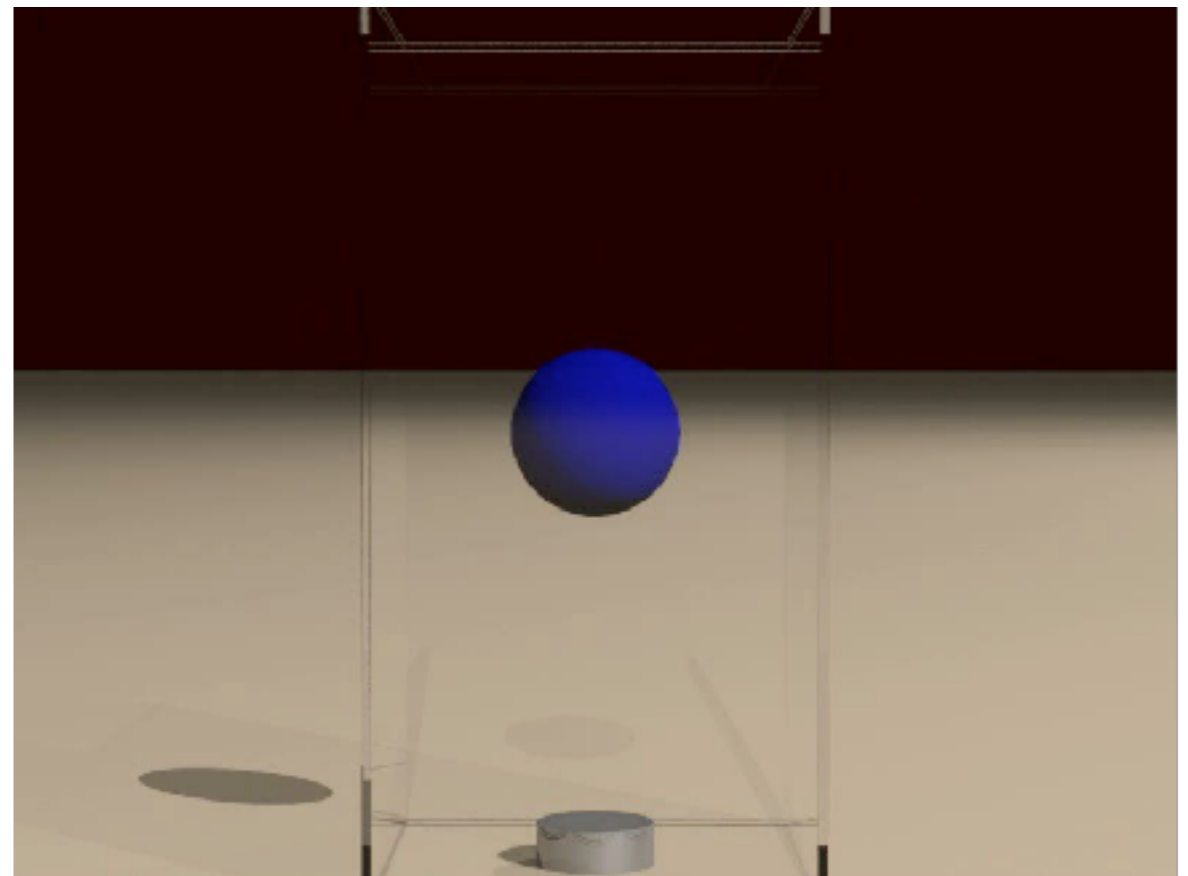
Smoke simulation

Scalar fields c : smoke density, T : (relative) temperature

1. Update $c^{n+1} = \text{advect}(c^n, \mathbf{u}^n, \Delta t)$,
 $T^{n+1} = \text{advect}(T^n, \mathbf{u}^n, \Delta t)$

2. Add buoyancy force:

$$\mathbf{f}_{\text{ext}} += (-\alpha c^{n+1} + \beta T^{n+1}) \hat{\mathbf{z}}$$



[Lentine et al. 2010]

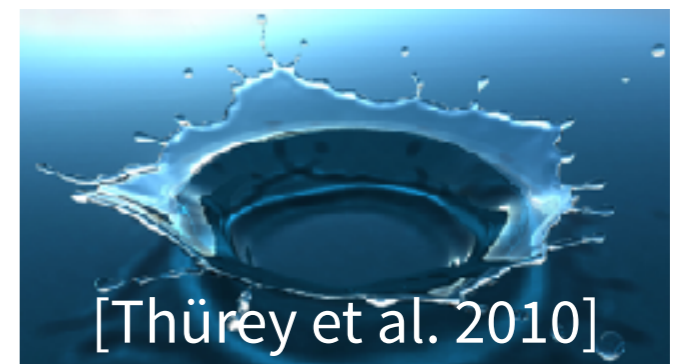
Issues

- ***Numerical dissipation***

- Diffusion in advection (almost eliminated by FLIP, APIC)
- Energy loss in projection [see Zhang et al. 2015, Zehnder et al. 2018]

- ***Boundary handling***

- Sloped solid boundaries [Batty et al. 2007]
- Liquid surfaces (next up)
- Small features (thin boundaries, fluid sheets, splashes) require hybrid methods



Liquids

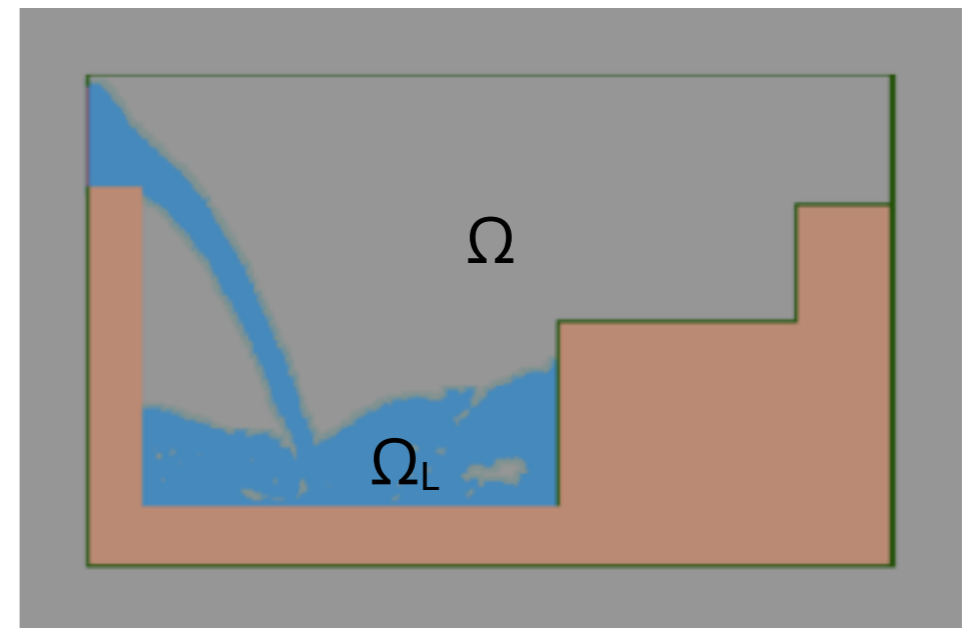
Liquids

What's the difference between liquids and gases (in our model)?

Liquid region does not fill entire domain.

Liquid/air boundary is a **free surface** that moves with fluid velocity \mathbf{u}

- How to represent liquid region?
- How to modify eqs. of motion?



[Foster & Metaxas 1996]

Surface tracking

What we need:

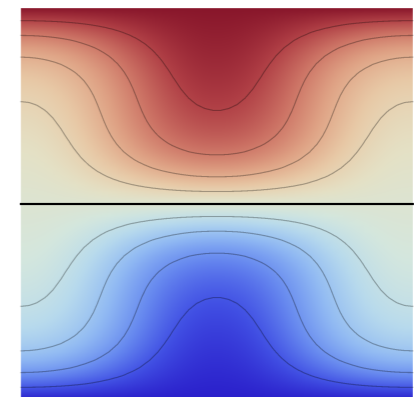
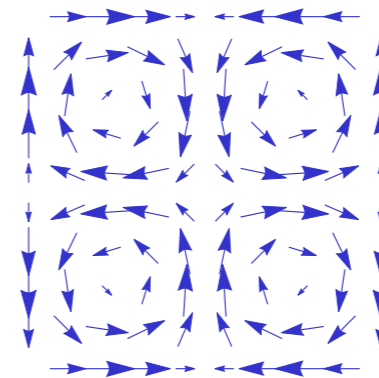
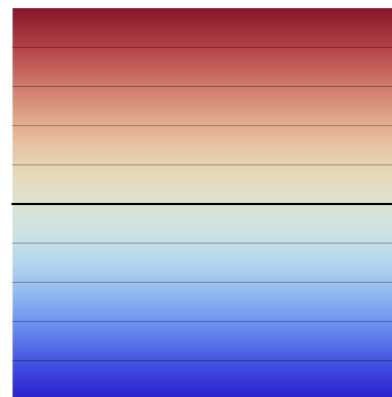
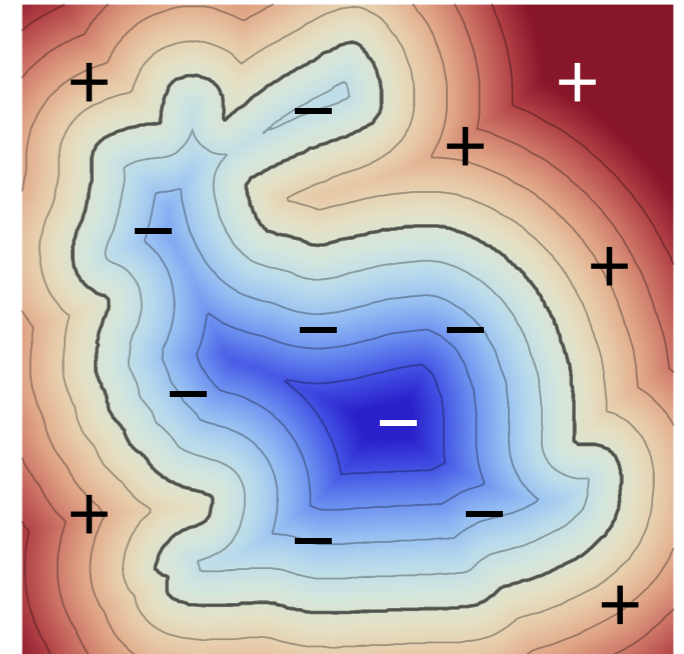
- Determine whether cell is *inside / outside* liquid
- ***Advect*** through velocity field
- ***Reconstruct*** surface for rendering

Level sets

[Foster & Fedkiw 2001, Bridson & Müller-Fischer Ch 6.2]

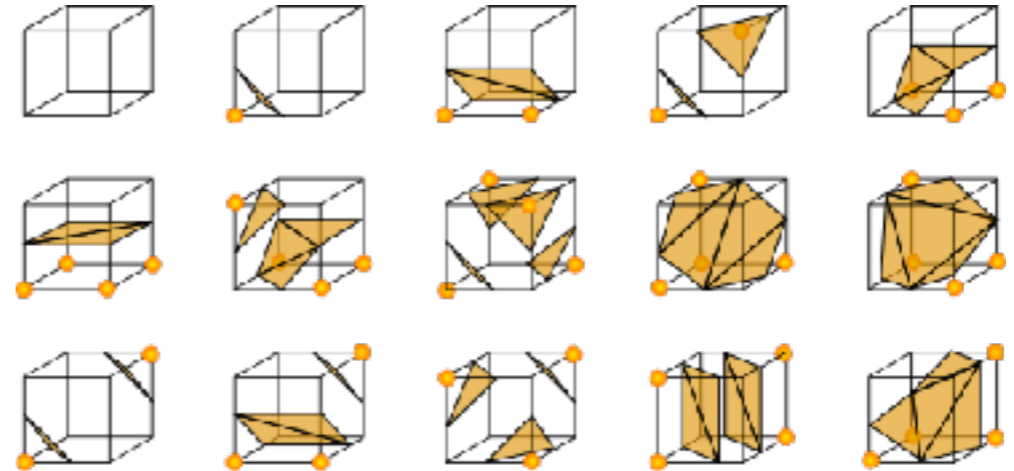
Represent region as sublevel set of scalar field φ , usually ***signed distance function***

- $\varphi < 0$ inside, $\varphi > 0$ outside,
 $|\varphi| = \text{distance to surface}$
- ***Inside/outside***: Just check sign of φ
- ***Advection***: Advect φ as scalar field, then do “redistancing”
 - Fast marching, fast sweeping methods



Level sets

- **Reconstruction:** Marching cubes



Advantages:

- Automatically handles topology changes

Disadvantages:

- Diffusion causes loss of volume & surface detail
- Requires periodic redistancing

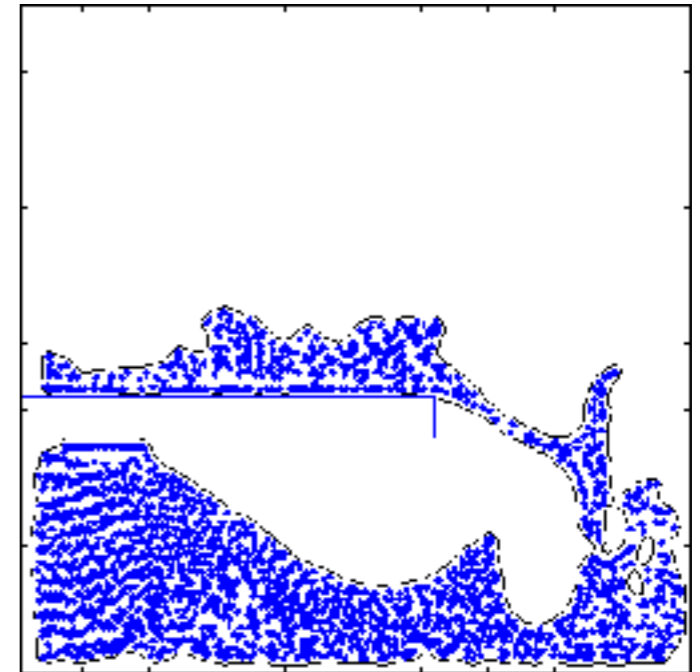
Particles

Place particles around the surface

[Enright et al. 2002] or everywhere in liquid

[Foster & Metaxas 1996, Zhu & Bridson 2005]

- **Advection** is trivial: just move particles
- **Inside/outside**: Mark cell as fluid if it contains **any** particles
- **Reconstruction**: Construct an SDF φ , then marching cubes (or directly render with ray tracing)
 - Most common approach: distance from “average neighbour”
 $\varphi(\mathbf{x}) = \|\mathbf{x} - \bar{\mathbf{x}}\| - \bar{r}$ [Zhu & Bridson 2005, Adams et al. 2007]



[Zhu & Bridson 2005]

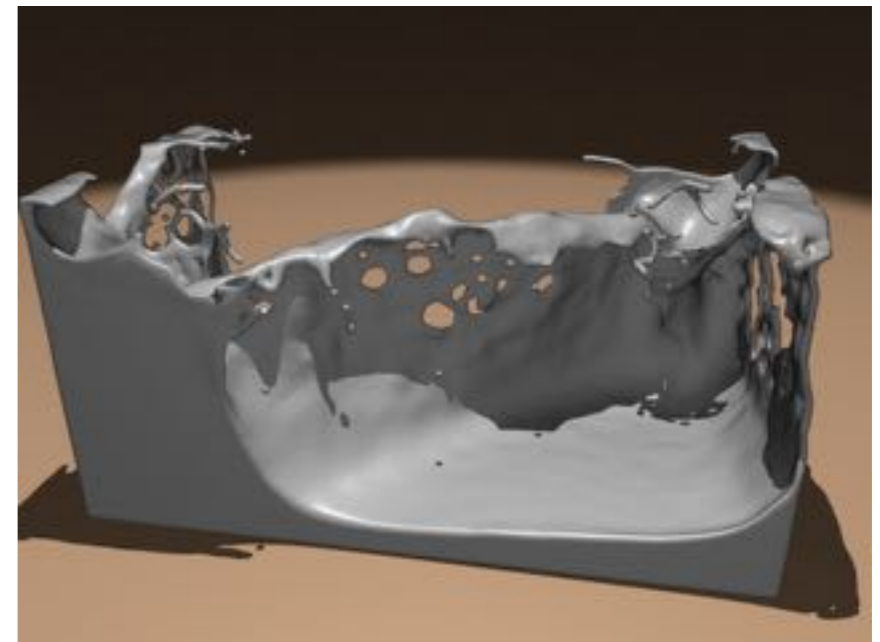
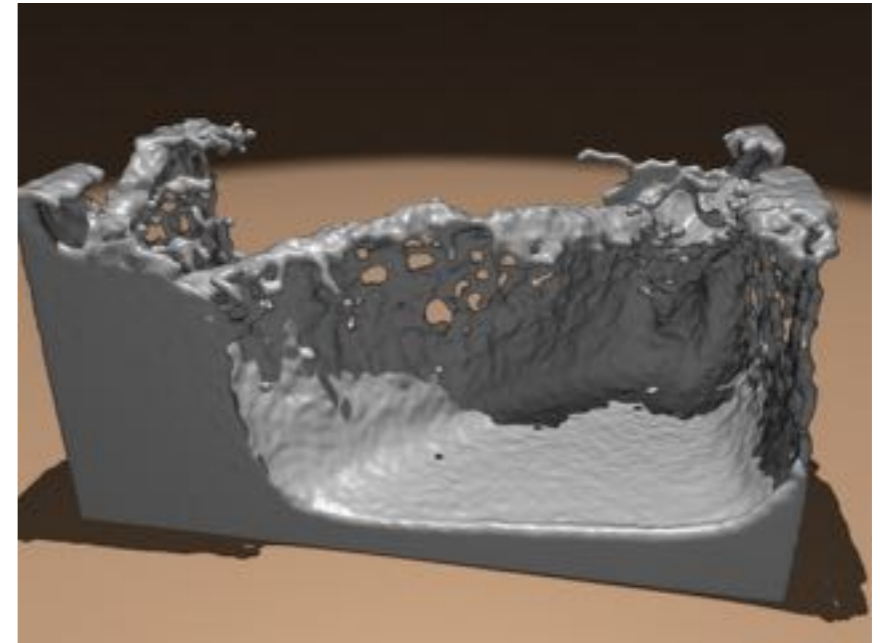
Particles

Advantages:

- Handles topology changes
- Better preserves volume
- Automatically produces droplets at splashes

Disadvantages:

- Bumpy surfaces
- Sheets tend to break up into droplets

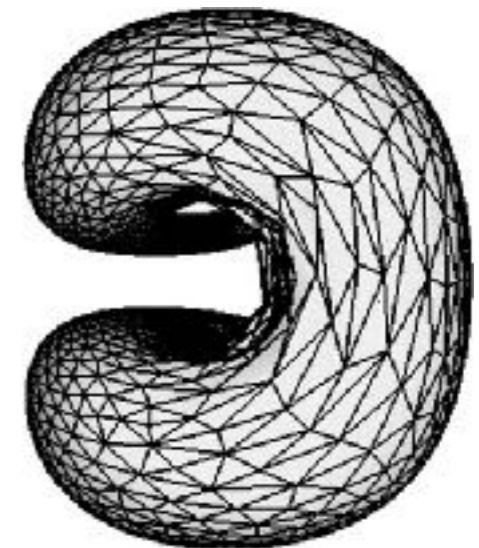


[Yu & Turk 2010]

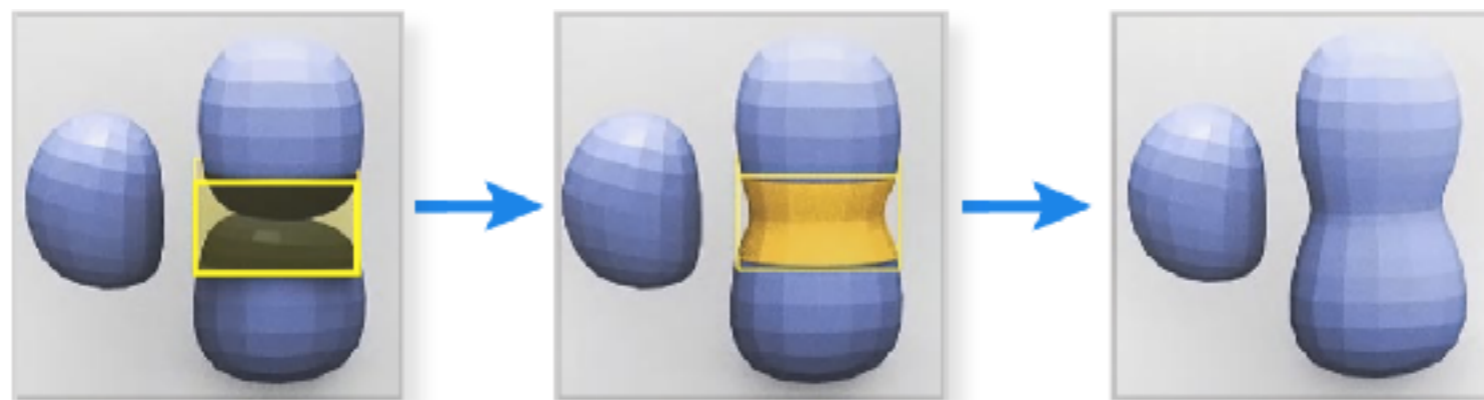
Meshes

Store surface explicitly as triangle mesh [Wojtan et al. 2011]:
no reconstruction necessary

- **Inside/outside:** Ray casting
- **Advection:** Move vertices (easy),
then improve mesh (hard!)
 - Modify stretched/squashed triangles,
deal with merging and splitting



[Brochu & Bridson 2009]



[Wojtan et al. 2009]

Meshes

Advantages:

- Highly accurate surfaces, great for surface tension effects
- Liquid sheets well preserved

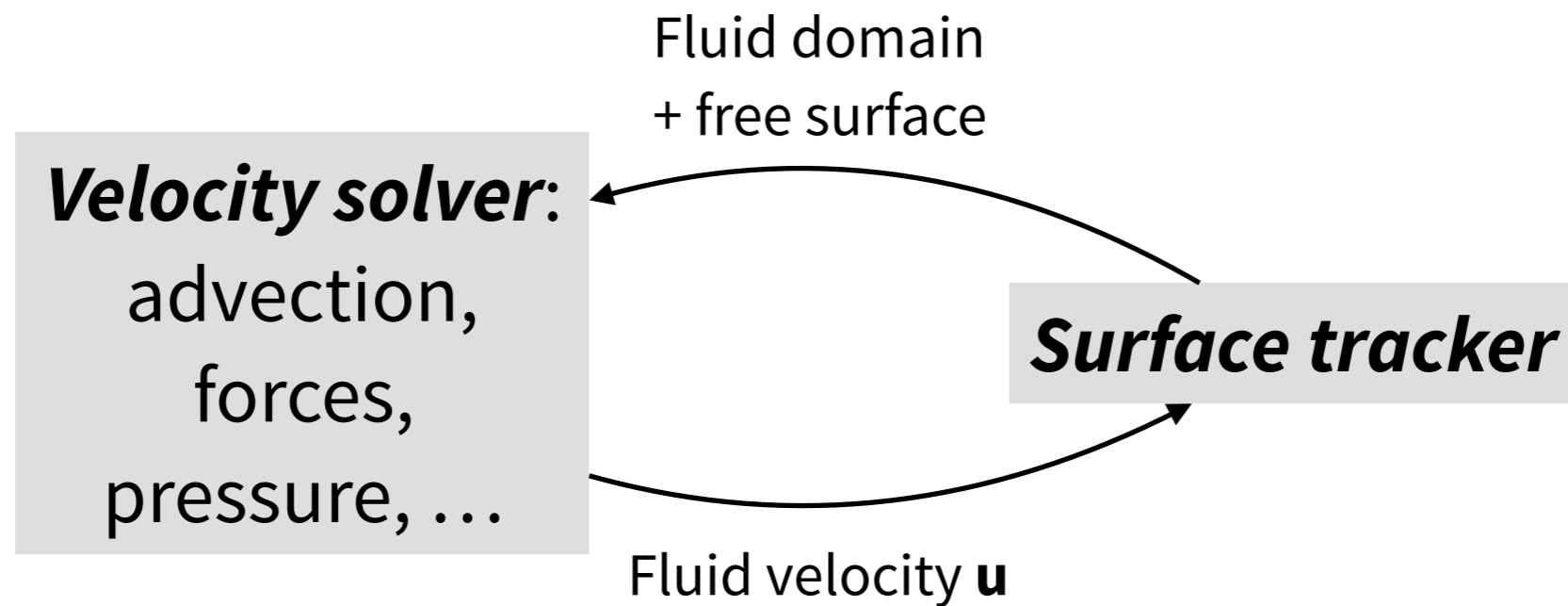
Disadvantages:

- Much more complicated to implement
- Grid dynamics may not “see” all the surface details



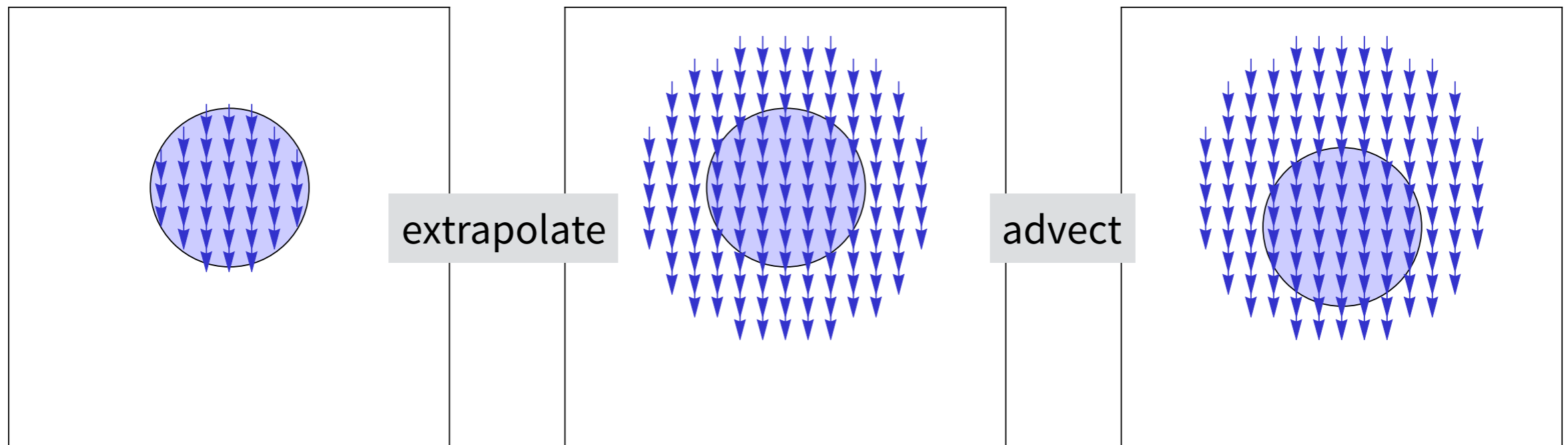
[Goldade et al. 2016]

Surface dynamics



Velocity extrapolation

Advection may query velocities *outside* current liquid region



Set $\mathbf{u}(\text{air}) = \mathbf{u}(\text{nearest fluid cell})$, similar to fast marching

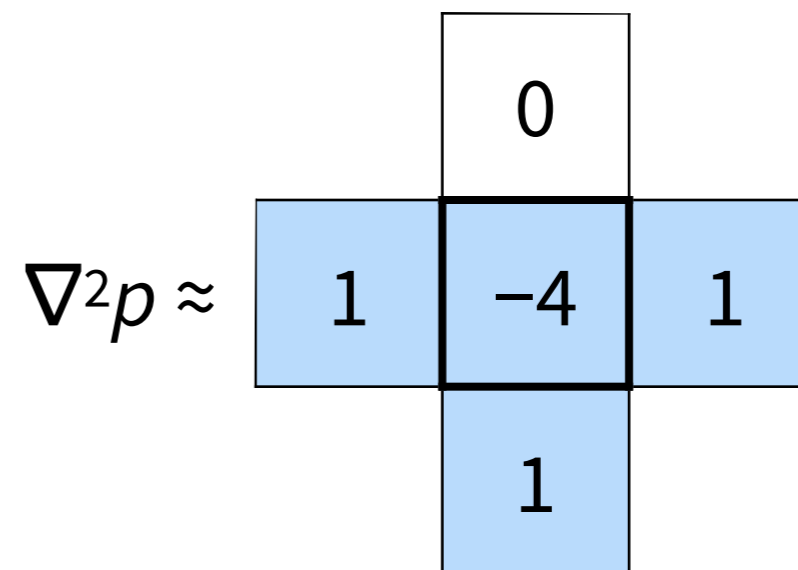
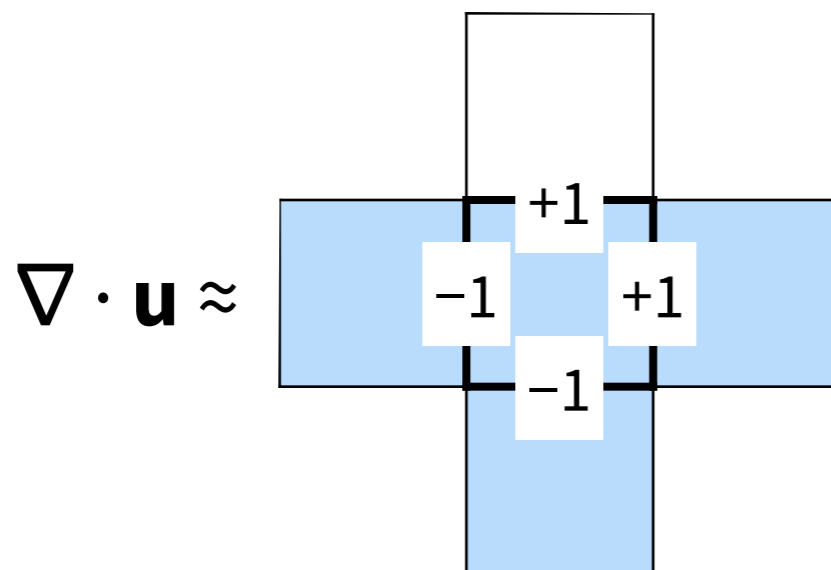
Free surface boundary conditions

Assume air is at **constant** atmospheric pressure $p = p_{\text{atm}}$
(Dirichlet boundary condition)

- Can assume $p_{\text{atm}} = 0$ (Why?)

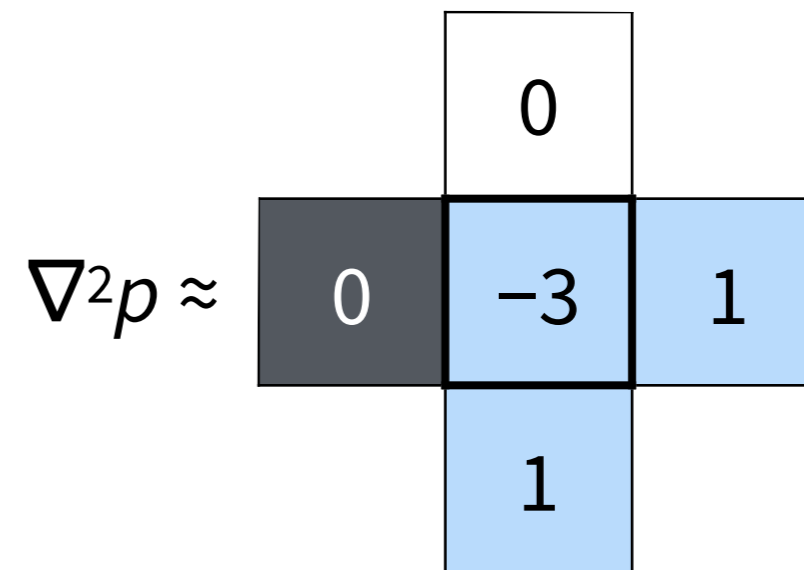
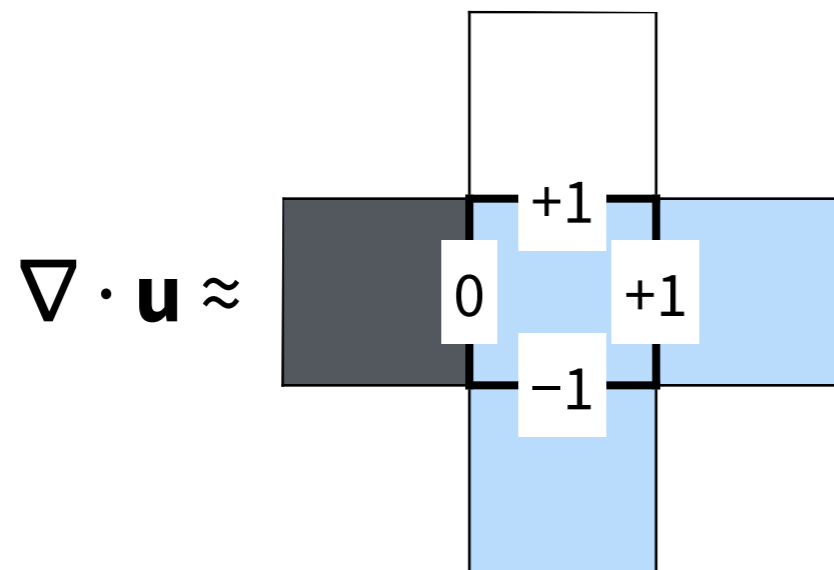
Air cells drop out of Laplacian formula, e.g.

$$(\nabla^2 p)_{i,j} \approx (p_{i-1,j} + p_{i+1,j} + p_{i,j-1} + \cancel{p_{i,j+1}} - 4 p_{i,j}) / \Delta x^2 = 0$$

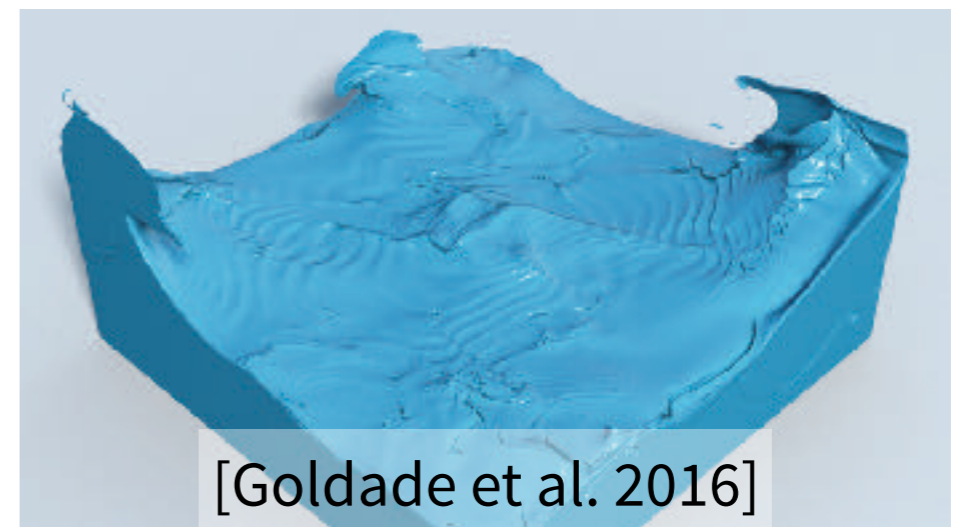


Free surface boundary conditions

With both solid and air neighbours:



Sloped surfaces: [Gibou et al. 2002]
See Bridson & Müller-Fischer Ch 4.5.1



Surface tension

surface tension coefficient

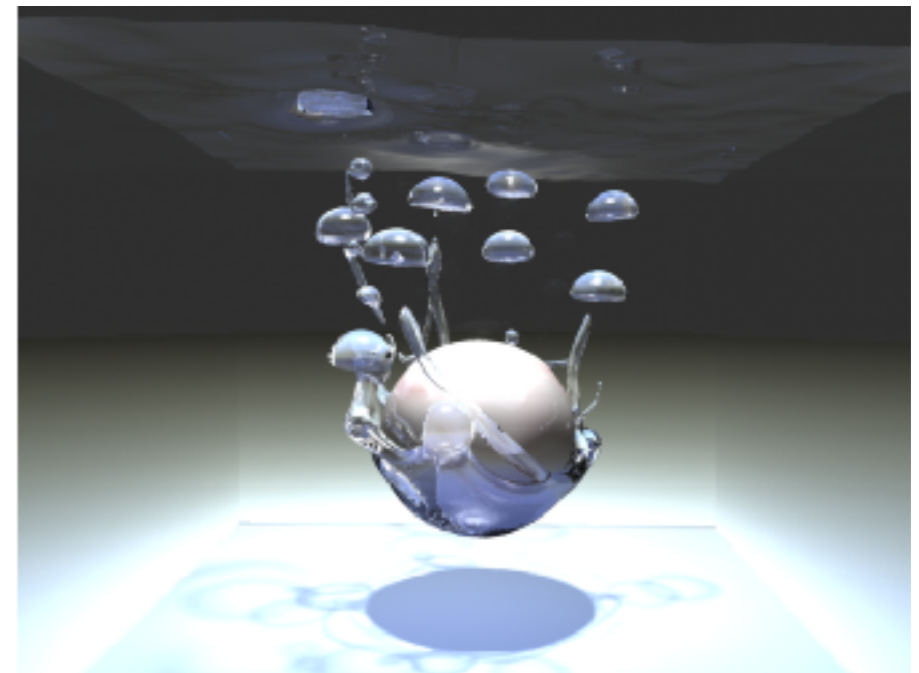
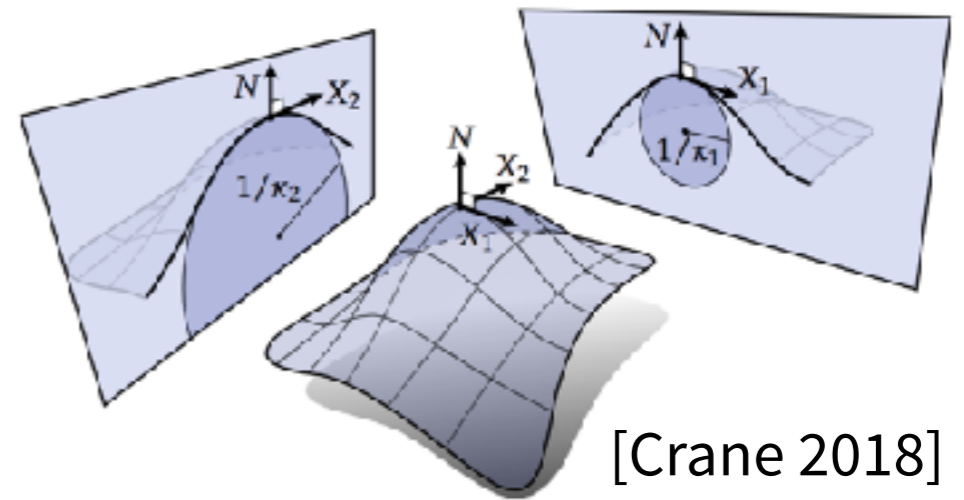
Theory: force per unit area = $2 \gamma H \hat{n}$
where $H = (K_1 + K_2)/2$: mean curvature

One approach [Hong & Kim 2005]:

- Compute K from SDF
- Apply pressure boundary condition

$$p = p_{\text{atm}} + 2 \gamma H$$

Problem: surface tension forces
computed explicitly
 \Rightarrow time step restriction



[Hong & Kim 2005]

Next class

Fluid simulation with particles alone:
Smoothed particle hydrodynamics

Readings:

- Müller et al., “Particle-Based Fluid Simulation for Interactive Applications”, 2003
- Becker & Teschner, “Weakly Compressible SPH for Free Surface Flows”, 2007

